Adjoint Sensitivity Analysis for Two Layered Shallow Water Equations

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August 18, 2009

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Adjoint Sensitivity Analysis

08/18/2009 1 / 33

Organization of the talk

- Motivation and Literature Survey
- Direct Sensitivity Method
- Adjoint Sensitivity Method
- Adjoint Sensitivity Analysis for two layered shallow water equations
 - Shallow water approximation for two layered sea
 - Normal form and its adjoint
 - Standard Adjoint Formalism
 - Characteristic Adjoint Formalism
- Summary

Motivation and Literature Survey

- J.J. Stoker Water Waves The Mathematical Theory with Applications Pure and Applied Mathematics Vol. IV (1957).
- N.D. Katopodes Two dimensional unsteady flow through a breached dam by the method of characteristics, Ph.D. Thesis (1977).
- Marchuk Adjoint Equations and Analysis of Complex Systems (1995).
- B.F. Sanders Control of shallow-water flow using the adjoint sensitivity method, Ph.D. Thesis (1997).
- B. F. Sanders and N.D. Katopodes Adjoint sensitivity analysis for shallow-water wave control J of Engineering Mechanics (2000).
- P. Concus, G.H. Golub and Y. Sun *Object-oriented parallel algorithms for computing three-dimensional isopycnal flow* International Journal for Numerical Methods in Fluids (2002).
- A. Rousseau, R. Temam and J. Tribbia Numerical simulations of the inviscid primitive equations in a limited domain Advances in Mathematical Fluid Dynamics (2006).

Why an Adjoint Equation?

Diffusion equation defined in the domain $x \in (0, L)$ is

$$D\frac{\partial^2 C}{\partial x^2} + f = 0, \ C(0) = C(L) = 0$$

Objective function :

$$J = \int_0^L r(x)C(x)\,dx$$

where $r = \delta(x - x_T)$.

Adjoint Equation

$$D\frac{\partial^2 C^*}{\partial x^2} + r = 0$$

Objective function:

$$J = \int_0^L f(x) C^*(x) \, dx$$

where $f = M\delta(x - x_s)$.

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Derivation

$$\int_{0}^{L} C^{*} \left[D \frac{\partial^{2} C}{\partial x^{2}} + f \right] dx = D \left[C^{*} \frac{\partial C}{\partial x} \right]_{0}^{L} - D \left[\frac{\partial C^{*}}{\partial x} C \right]_{0}^{L} + \int_{0}^{L} \left[C D \frac{\partial^{2} C^{*}}{\partial x^{2}} + C^{*} f \right] dx = 0$$

$$J = \int_0^L \left[CD \frac{\partial^2 C^*}{\partial x^2} + C^* f \right] dx + \int_0^L r C dx$$

 $J = \int_0^L C\left[D\frac{\partial^2 C^*}{\partial x^2} + r\right] dx + \int_0^L fC^* dx$

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Shallow Water Equations

$$\frac{\partial \eta}{\partial t} + \frac{\partial (Hu' + \bar{U}\eta)}{\partial x} = 0$$
$$\frac{\partial u'}{\partial t} + \frac{\partial (\bar{U}u' + g\eta)}{\partial x} = 0$$

Objective Function

$$J = \int_0^T \int_0^L r(\eta, u'; x, t) dx dt$$

t = time; x = distance along the channel; η = flow perturbation; u' = discharge per unit width; r = user-defined measuring function

$$r = \frac{1}{2} \left[\eta(x_0, t) - \bar{\eta}(x_0) \right]^2 \delta(x - x_0)$$

Direct Sensitivity Method

- The basic problem is solved
- A reference value of the objective function J_0 is computed
- A flow variable is perturbed at the boundary at the selected perturbation time
- The associated objective function value is computed again
- This procedure is repeated for sufficiently many selections of time
- This yields the temporal evolution of the sensitivities

Adjoint Sensitivity Method

Derivation of 1D Adjoint Equations

- Adjoint variables : $\phi(x, t)$ and $\psi(x, t)$
- Multiply the continuity equation by $\phi(x, t)$ and the momentum equation by $\psi(x, t)$
- The sum of these two products is then integrated over space and time
- Flow control is desired
- \bullet Variation of the objective function with respect to η and u' is calculated
- Add these two variations
- Assign initial condition for the adjoint problem
- Assign boundary values for the adjoint variables

Sensitivity Equations

- Sensitivities required for subcritical flow control are given by $\frac{\delta J}{\delta u'(0,t)}$ and $\frac{\delta J}{\delta \eta(L,t)}$
- Sensitivities required for supercritical flow control are given by $\frac{\delta J}{\delta u'(0,t)}$ and $\frac{\delta J}{\delta \eta(0,t)}$
- To derive expressions for sensitivities in terms of the adjoint variables
- Initial condition for the basic problem $\eta(x,0) = \eta_0(x), u'(x,0) = u'_0(x); \delta\eta(x,0) = 0, \delta u'(x,0) = 0$
- Initial conditions in the adjoint problem $\phi(x, T) = 0 = \psi(x, T)$
- Selection of boundary conditions for the adjoint problem is motivated by the boundary conditions of the basic problem
- Expressions are then derived for sensitivities to these boundary values

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Shallow water equations and its Adjoint

$$\frac{\partial \eta}{\partial t} + \bar{U}\frac{\partial \eta}{\partial x} + \bar{V}\frac{\partial \eta}{\partial y} + H\frac{\partial u'}{\partial x} + H\frac{\partial v'}{\partial y} = 0$$
$$\frac{\partial u'}{\partial t} + \bar{U}\frac{\partial u'}{\partial x} + \bar{V}\frac{\partial u'}{\partial y} + g\frac{\partial \eta}{\partial x} = 0$$
$$\frac{\partial v'}{\partial t} + \bar{U}\frac{\partial v'}{\partial x} + \bar{V}\frac{\partial v'}{\partial y} + g\frac{\partial \eta}{\partial y} = 0$$

Adjoint

$$\begin{aligned} \frac{\partial \phi}{\partial \tau} &- \bar{U} \frac{\partial \phi}{\partial x} - \bar{V} \frac{\partial \phi}{\partial y} - g \frac{\partial \psi_1}{\partial x} - g \frac{\partial \psi_2}{\partial y} + \frac{\partial r}{\partial \eta} &= 0\\ \frac{\partial \psi_1}{\partial \tau} &- \bar{U} \frac{\partial \psi_1}{\partial x} - \bar{V} \frac{\partial \psi_1}{\partial y} - H \frac{\partial \phi}{\partial x} + \frac{\partial r}{\partial u'} &= 0\\ \frac{\partial \psi_2}{\partial \tau} &- \bar{U} \frac{\partial \psi_2}{\partial x} - \bar{V} \frac{\partial \psi_2}{\partial y} - H \frac{\partial \phi}{\partial y} + \frac{\partial r}{\partial v'} &= 0 \end{aligned}$$

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Nonreflective Outflow Boundary

Adjoint boundary conditions:

 $\psi(0,t)=0$ and $\phi(L,t)+2rac{u'(L,t)}{\eta(L,t)}\psi(L,t)=0$

Sensitivities for the subcritical flow then are:

$$\frac{\delta J}{\delta u'(0, t_p)} = \phi(0, t_p)$$

$$\frac{\delta J}{\delta \eta(L, t_p)} = \left[\left(\frac{u'(L, t_p)}{\eta(L, t_p)} \right)^2 - g \eta(L, t_p) \right] \psi(L, t_p)$$

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A two layered sea of constant depth



Two layered Shallow water model

The two layered shallow water model is given by,

$$\frac{\partial \eta_1}{\partial t} + \frac{\partial}{\partial x} \left[(\eta_1 - \eta_0) u_1 \right] = 0$$
$$\frac{\partial u_1}{\partial t} + \frac{\partial}{\partial x} \left[\frac{u_1^2}{2} + ga\eta_1 + gb\eta_2 \right] = 0$$

for the lower layer and

$$\frac{\partial \eta_2}{\partial t} + \frac{\partial}{\partial x} \left[(\eta_1 - \eta_0) u_1 + (\eta_2 - \eta_1) u_2 \right] = 0$$
$$\frac{\partial u_2}{\partial t} + \frac{\partial}{\partial x} \left[\frac{u_2^2}{2} + gb\eta_2 \right] = 0$$

for the upper layer where $a = \frac{(\rho_1 - \rho_2)}{\rho_0}$ and $b = \frac{\rho_2}{\rho_0}$ and $u_1 = u_1(x, t)$ and $u_2 = u_2(x, t)$ are the velocity components, $\eta_1 = \eta_1(x, t)$ and $\eta_2 = \eta_2(x, t)$ are perturbations of the height field for lower and upper layers respectively. The problem is defined in limited domain ie., $0 \le x \le L$.

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Adjoint Sensitivity Analysis

Barotropic and Baroclinic Modes

The linearized two layered shallow water model in normal form is given by,

$$\frac{\partial \zeta}{\partial t} + \left(\frac{h+h'}{h}\right) \frac{\partial U}{\partial x} = 0$$
$$\frac{\partial U}{\partial t} + gh \frac{\partial \zeta}{\partial x} = 0$$
$$\frac{\partial \zeta'}{\partial t} + \frac{\partial U'}{\partial x} = 0$$
$$\frac{\partial U'}{\partial t} + \left(\frac{g\epsilon hh'}{h+h'}\right) \frac{\partial \zeta'}{\partial x} = 0$$

This is in barotropic and baroclinic modes. Here, $\epsilon = \frac{\rho' - \rho}{\rho'}$. Initial conditions for the Direct Problem:

$$\zeta(x,0) = \zeta_0(x); \zeta'(x,0) = \zeta'_0(x); U(x,0) = U_0(x); U'(x,0) = U'_0(x)$$

$$\delta\zeta(x,0) = 0; \ \delta\zeta'(x,0) = 0; \ \delta U(x,0) = 0; \ \delta U'(x,0) = 0$$



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08/18/2009 15 / 33



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08/18/2009 16 / 33



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08/18/2009 17 / 33



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The Adjoint

The adjoint for the normal form of two layered shallow water equations (in barotropic and baroclinic modes) is given by,

$$\frac{\partial \phi}{\partial \tau} - gh \frac{\partial \psi}{\partial x} + \frac{\partial r}{\partial \zeta} = 0$$

$$\frac{\partial \psi}{\partial \tau} - \left(\frac{h+h'}{h}\right) \frac{\partial \phi}{\partial x} + \frac{\partial r}{\partial U} = 0$$

$$\frac{\partial \phi'}{\partial \tau} - gh' \frac{\partial \psi'}{\partial x} + \frac{\partial r}{\partial \zeta'} = 0$$

$$\frac{\partial \psi'}{\partial \tau} - \left(\frac{h+h'}{h'}\right) + \frac{\partial r}{\partial U'} = 0$$

Initial conditions for the Adjoint Problem:

$$\phi(x, T) = 0; \ \phi'(x, T) = 0; \ \psi(x, T) = 0; \ \psi'(x, T) = 0$$

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Standard Adjoint Problem Formalism

Boundary Conditions:

$$\phi(L,t) = \zeta(L,t); \ \psi(0,t) = U(0,t); \quad \phi'(L,t) = \zeta'(L,t); \ \psi'(0,t) = U'(0,t)$$

$$\delta J = \int_0^T \left[a\phi(L,t)\delta U + b\psi(L,t)\delta\zeta + c\phi'(L,t)\delta U' + d\psi'(L,t)\delta\zeta' \right]_0^L dt$$

Sensitivities:

$$\frac{\delta J}{\delta U(0,t_p)} = -a\phi(0,t_p); \quad \frac{\delta J}{\delta U'(0,t_p)} = -c\phi'(0,t_p)$$
$$\frac{\delta J}{\delta \zeta(L,t_p)} = b\psi(L,t_p); \quad \frac{\delta J}{\delta \zeta'(L,t_p)} = d\psi'(L,t_p)$$

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08/18/2009 20 / 33

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 22 / 33



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Adjoint Sensitivity Analysis



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Transformation of Direct Equations

$$\frac{\partial W}{\partial t} + A \frac{\partial W}{\partial x} = 0$$

where

$$W = \begin{pmatrix} \zeta \\ U \\ \zeta' \\ U' \end{pmatrix}, \quad A = \begin{bmatrix} 0 & a & 0 & 0 \\ b & 0 & 0 & 0 \\ 0 & 0 & 0 & c \\ 0 & 0 & d & 0 \end{bmatrix}$$

with $a = \frac{(h+h')}{h}$, $b = gh$, $c = 1$ and $d = \frac{g\epsilon hh'}{h+h'}$.

The eigenvalues of A are given by, $\lambda_1 = -\sqrt{ab}, \ \lambda_2 = \sqrt{ab}, \ \lambda_3 = -\sqrt{cd}, \ \lambda_4 = \sqrt{cd}.$

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Transformation of Direct Equations

The matrix of right and left eigenvectors are then given by,

$$RE = \begin{pmatrix} -\sqrt{\frac{a}{b}} & 1 & 0 & 0\\ \sqrt{\frac{a}{b}} & 1 & 0 & 0\\ 0 & 0 & -\sqrt{\frac{c}{d}} & 1\\ 0 & 0 & \sqrt{\frac{c}{d}} & 1 \end{pmatrix}$$
$$LE = \frac{1}{2} \begin{pmatrix} -\sqrt{\frac{b}{a}} & \sqrt{\frac{b}{a}} & 0 & 0\\ 1 & 1 & 0 & 0\\ 0 & 0 & -\sqrt{\frac{d}{c}} & \sqrt{\frac{d}{c}}\\ 0 & 0 & 1 & 1 \end{pmatrix}$$

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Characteristics for Direct Equations

$$C^{1} : \frac{d\zeta}{dt} - \frac{dU}{dt} = 0 \text{ along } \frac{dx}{dt} = -\sqrt{ab}$$

$$C^{2} : \frac{d\zeta}{dt} + \frac{dU}{dt} = 0 \text{ along } \frac{dx}{dt} = \sqrt{ab}$$

$$C^{3} : \frac{d\zeta'}{dt} - \frac{dU'}{dt} = 0 \text{ along } \frac{dx}{dt} = -\sqrt{cd}$$

$$C^{4} : \frac{d\zeta'}{dt} + \frac{dU'}{dt} = 0 \text{ along } \frac{dx}{dt} = \sqrt{cd}$$

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Transformation of Adjoint Equations

$$\Phi_{\tau} + \tilde{A}\Phi_{x} + \tilde{R} = 0$$

where

$$\Phi = \begin{pmatrix} \phi \\ \psi \\ \phi' \\ \psi' \end{pmatrix}, \quad A = \begin{bmatrix} 0 & -b & 0 & 0 \\ -a & 0 & 0 & 0 \\ 0 & 0 & 0 & -d \\ 0 & 0 & -c & 0 \end{bmatrix}, \quad \tilde{R} = \begin{pmatrix} \frac{\partial r}{\partial \zeta} \\ \frac{\partial r}{\partial U} \\ \frac{\partial r'}{\partial \zeta'} \\ \frac{\partial r}{\partial U'} \end{pmatrix}$$

with $a = \frac{(h+h')}{h}$, b = gh, c = 1 and $d = \frac{-g\epsilon hh'}{h+h'}$. The eigenvalues of \tilde{A} are given as,

$$\lambda_1 = -\sqrt{g(h+h')}, \ \lambda_2 = \sqrt{g(h+h')}, \ \lambda_3 = -\sqrt{rac{g\epsilon hh'}{h+h'}}, \ \lambda_4 = \sqrt{rac{g\epsilon hh'}{h+h'}}$$

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Transformation of Adjoint Equations

The matrix of right and left eigenvectors are then given as,

$$RE = \begin{pmatrix} \sqrt{\frac{b}{a}} & 1 & 0 & 0\\ -\sqrt{\frac{b}{a}} & 1 & 0 & 0\\ 0 & 0 & \sqrt{\frac{d}{c}} & 1\\ 0 & 0 & -\sqrt{\frac{d}{c}} & 1 \end{pmatrix}$$
$$LE = \frac{1}{2} \begin{pmatrix} \sqrt{\frac{a}{b}} & -\sqrt{\frac{a}{b}} & 0 & 0\\ 1 & 1 & 0 & 0\\ 0 & 0 & \sqrt{\frac{c}{d}} & -\sqrt{\frac{c}{d}}\\ 0 & 0 & 1 & 1 \end{pmatrix}$$

and

Characteristics for Adjoint Equations

$$C^{1} : \frac{d\phi}{d\tau} - \frac{d\psi}{d\tau} + \frac{\partial r}{\partial \zeta} - \frac{\partial r}{\partial U} = 0 \quad \text{along} \quad \frac{dx}{d\tau} = -\sqrt{ab}$$

$$C^{2} : \frac{d\phi}{d\tau} + \frac{d\psi}{d\tau} + \frac{\partial r}{\partial \zeta} + \frac{\partial r}{\partial U} = 0 \quad \text{along} \quad \frac{dx}{d\tau} = \sqrt{ab}$$

$$C^{3} : \frac{d\phi'}{d\tau} - \frac{d\psi'}{d\tau} + \frac{\partial r}{\partial \zeta'} + \frac{\partial r}{\partial U'} = 0 \quad \text{along} \quad \frac{dx}{d\tau} = -\sqrt{cd}$$

$$C^{4} : \frac{d\phi'}{d\tau} + \frac{d\psi'}{d\tau} + \frac{\partial r}{\partial \zeta'} + \frac{\partial r}{\partial U'} = 0 \quad \text{along} \quad \frac{dx}{d\tau} = \sqrt{cd}$$

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Characteristic Adjoint Formalism

To obtain sensitivity expressions for U and U' at upstream and downstream, we substitute the above characteristics in δJ , we get

$$\frac{\delta J}{\delta U(0,t_p)} = -\frac{h+h'}{h}\phi(0,t_p) + gh\psi(0,t_p)$$
$$\frac{\delta J}{\delta U'(0,t_p)} = -\phi'(0,t_p) + \frac{g\epsilon hh'}{h+h'}\psi'(0,t_p)$$
$$\frac{\delta J}{\delta U(L,t_p)} = \frac{h+h'}{h}\phi(L,t_p) + gh\psi(L,t_p)$$
$$\frac{\delta J}{\delta U'(L,t_p)} = \phi'(L,t_p) + \frac{g\epsilon hh'}{h+h'}\psi'(L,t_p)$$

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Characteristic Adjoint Formalism

Similarly by substituting the above characteristics, we can also obtain the sensitivity expressions for height field at both the upstream and downstream as,

$$\frac{\delta J}{\delta \zeta(0, t_p)} = \frac{h+h'}{h} \phi(0, t_p) - gh\psi(0, t_p)$$
$$\frac{\delta J}{\delta \zeta'(0, t_p)} = \phi'(0, t_p) - \frac{g\epsilon h'h}{h+h'} \psi'(0, t_p)$$
$$\frac{\delta J}{\delta \zeta(0, t_p)} = h+h'$$

and

$$\frac{\delta J}{\delta \zeta(L, t_p)} = \frac{h + h'}{h} \phi(L, t_p) + gh\psi(L, t_p)$$
$$\frac{\delta J}{\delta \zeta'(L, t_p)} = \phi'(L, t_p) + \frac{g\epsilon h h'}{h + h'} \psi'(L, t_p)$$



Characteristic adjoint sensitivity analysis for transient motion in a two-layered sea

- To determine how a specific condition is dependent on many parameters which influence it
- Adjoint sensitivity method is more efficient than Direct sensitivity method
- Fast and accurate tool for computing the sensitivities
- Characteristic adjoint sensitivity method gives better results than Standard adjoint sensitivity method
- Boundary conditions derived for linear approximation can be used for the nonlinear problem
- Numerical work in progress