



Conservative Cascade Interpolation on the Sphere: An Intercomparison of Various Non-Oscillatory Reconstructions

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Abstract: Various new polynomial and non-polynomial approximations to subgrid distribution have been adapted for use in the conservative cascade scheme (CCS) and applied to conservative grid-to-grid interpolation on a latitude-longitude grid. These approximations include the following: Piecewise Parabolic Method (PPM), Piecewise Hyperbolic Method (PHM), Piecewise Double Hyperbolic Method (PDHM), Power-limited Piecewise Parabolic Method (P-PPM), Piecewise Rational Method (PRM), third-order Weighted Essentially Non-Oscillatory (WENO23), fifth-order Weighted Essentially Non-Oscillatory (WENO35), and a Modified Piecewise Parabolic Method (M-PPM). A series of test cases are performed in which initial gridded data is interpolated between T42 and 2° grids and compared against analytical values. Four initial data profiles are used: smooth harmonic, high frequency harmonic, quasi-polar vortex data, and slotted cylinder data. In general, PDHM (WENO35) had the lowest error norms of the three- (five-)cell stencil methods. Quite often, M-PPM gave accuracy comparable to WENO35 at significantly lower cost. Monotonicity violations generally only occurred when interpolating to a finer grid with a maximum violation of 1.8. Copyright © 2008 Royal Meteorological Society

KEY WORDS

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1 Introduction

Conservative remapping involves accurately transferring data from one grid to another while conserving the global and local integrals. Methods currently existing in the literature for meteorological application include Jones (1999), Lauritzen and Nair (2008), and Ulrich *et al.* (2009). The basic conservative interpolation steps of Nair *et al.* (2002) and Zerroukat *et al.* (2004) and can also be used for geophysical interpolation. The method of Jones (1999) is very flexible and is applicable to many spherical grids but is at most second-order accurate. Nair *et al.* (2002) and Zerroukat *et al.* (2004) employ a conservative cascade interpolation to calculate mass in departure cells for semi-Lagrangian advection on the sphere. Lauritzen and Nair (2008) apply the conservative cascade methodology for interpolation between regular latitude-longitude (RLL) grids and cubed-sphere grids. Ulrich *et al.* (2009) developed a novel fully two-dimensional approach to remapping between cubed-sphere and RLL grids which exactly integrates polynomial reconstructions via quadrature on cell boundaries. The primary focus of this study is on the relative performance of various one-dimensional non-oscillatory reconstructions, many of which have had little exposure to meteorological application. To this end, we choose the Conservative Cascade Scheme (CCS)

of Nair *et al.* (2002) and Norman and Nair (2008) as a framework testbed for this intercomparison.

Nair *et al.* (2002) and Norman and Nair (2008) applied the CCS to semi-Lagrangian (SL) transport on a RLL grid. Cascade interpolation is more efficient than a straightforward Cartesian splitting and involves fewer operations, especially for multiple species since the intermediate grid needs to be generated only once (see Purser and Leslie, 1991 and Nair *et al.*, 1999). The CCS also applies unchanged to the more general realm of geophysical grid-to-grid interpolation which has different computational challenges than SL transport. In the transport case, the scheme must be robust enough to handle a wide range of target grids as the wind flow varies in time. This is a notable difference from conservative interpolation in which the source and target grids are typically static. Also, for SL transport there must exist an equal number of source and target grid cells. This means the size of source and target grid cells on average are similar. In conservative interpolation there is no such restriction. There may be multiple target cells within every source cell and vice versa. In this study, the CCS is being applied to one step of conservative interpolation between two regular latitude-longitude grids. As in the transport case, non-oscillatory reconstructions during each 1-D CCS sweep ensure that the violation of monotonicity during the remapping is well controlled. Other techniques of conservative cascade remapping do exist such as in Zerroukat *et al.* (2004).

There are many applications of grid-to-grid interpolation in geophysical numerical simulation. For instance,

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the initial conditions and boundary conditions are always interpolated from data sets onto the model grid. Also, most components of an Earth system model are simulated on different grids, and when coupled interpolation between those grids is necessary. In adaptive mesh refinement (AMR), the grids are locally refined and coarsened, requiring interpolation between grids. Nothing precludes application to the restriction and prolongation operations in multigrid either for that matter. Also, as mentioned earlier, SL transport utilises an interpolation step in remapping mass from the static grid to the departure grid.

One general rule applies to all of these applications: The properties of the interpolation will propagate through the simulation. For example, a NWP forecast is forced mostly by initial conditions. Thus, if the initial conditions are inaccurately interpolated to the model grid, even high-order dynamical solvers will render inaccurate forecasts. The same can be said about climate simulations which are almost entirely boundary value problems due to their very long simulation times. With such high sensitivity to boundary specifications, a low-order accurate interpolation should not be coupled with high-order accurate dynamics. If the interpolation used when coupling two components isn't conservative, the overall simulation will not be conservative. If the interpolation used in AMR grid refinement is oscillatory, the simulation will exhibit oscillations. Therefore, if certain properties are desirable in a dynamical simulation, those same properties must be true of the interpolations used to transfer data from grid to grid.

The purpose of the present study is to perform an intercomparison of various functional approximations in the CCS applied to conservative interpolation between two latitude-longitude grids. These approximations include the Piecewise Parabolic Method and non-polynomial approximations from [Norman and Nair \(2008\)](#) as well as four new polynomial functions. The new reconstructions are the Power-limited Piecewise Parabolic Method (P-PPM), third-order Weighted Essentially Non-Oscillatory (WENO3) method, fifth-order Weighted Essentially Non-Oscillatory (WENO5) method, and a modified PPM (M-PPM). The M-PPM, developed in this study, uses a convex combination of the original full-order reconstruction and the classical limited reconstruction with the weighting defined by a mathematical indicator of jump discontinuity severity in the stencil.

There exist other polynomial interpolants in literature not included in this paper. For instance, [Zerroukat et al. \(2004\)](#) and [Zerroukat et al. \(2006\)](#) used piecewise cubic polynomials and quadratic splines, respectively, and both are limited by the filter provided in [Zerroukat et al. \(2005\)](#). These reconstructions are accurate, but cubics along with their filter require a wide stencil, and the splines require a global stencil. Small-stencil methods give an advantage in regard to scalability in that communication demand in parallel architectures is reduced compared to wide-stencil and global-stencil methods. Additionally, smaller stencil methods can be used closer to a material boundary (e.g. the Earth's surface) than wider

Acronym	Functional Approximation	Stencil
PPM	classical Piecewise Parabolic Method	5
P-PPM	Power-limited Piecewise Parabolic Method	3
WENO23	3 rd -order Weighted Essentially Non-Oscillatory	3
WENO35	5 th -order Weighted Essentially Non-Oscillatory	5
PHM	Piecewise Hyperbolic Method	3
PDHM	Piecewise Double Hyperbolic Method	3
PRM	Piecewise Rational Method	5
M-PPM	Modified Piecewise Parabolic Method	5

Table I. Functional approximations of this study, their respective acronyms, and the stencil size required. Here, stencil is defined as the total number of cells of information required for reconstruction of one cell (including the cell being reconstructed).

stencil methods. For this reason, we wish to restrict our attention to small-stencil methods, meaning the reconstruction of a cell requires a stencil of 5 cells or less (including the cell in question). Also, [Blossey and Durran \(2008\)](#) introduced a PPM variant wherein the classical limiter is only employed when a WENO-like parameter exceeds a certain threshold indicating a sufficiently large discontinuity. In fact, the M-PPM method developed in section 2.3 carries a similar approach: only limit the reconstruction to the degree to which it has the potential to cause oscillations.

The paper is organised as follows. Section 2 describes the sub-grid reconstructions, section 3 describes the test cases for the study, section 4 presents the numerical results, and conclusions are drawn in section 5.

2 Sub-grid Reconstructions

2.1 Non-Polynomial Reconstructions

For sake of brevity, the details of the non-polynomial reconstructions will not be reviewed in the present paper because they are implemented as described in [Norman and Nair \(2008\)](#) which describes them in detail. These reconstructions include the Piecewise Hyperbolic Method (PHM) of [Marquina \(1994\)](#) and [Serna \(2006\)](#), the Piecewise Double Hyperbolic Method (PDHM) of [Artebrant and Schroll \(2006\)](#), and the Piecewise Rational Method (PRM) of [Xiao et al. \(2002\)](#). For the reader's convenience, all functional approximations and their acronyms are defined in Table I along with the stencil required for each method. PHM and PDHM are implemented exactly as given in [Serna \(2006\)](#) and [Artebrant and Schroll \(2006\)](#), respectively. Additionally, PRM is implemented in this context with the same functional form as given in [Xiao et al. \(2002\)](#) with fourth-order accurate interface values following the PPM of [Colella and Woodward \(1984\)](#).

2.2 Power-limited Piecewise Parabolic Method (P-PPM)

The idea behind P-PPM is given in [Amat et al. \(2003\)](#), hereafter ABC03. The classical Piecewise Parabolic

Method (PPM) of [Colella and Woodward \(1984\)](#), which serves as a basis of comparison for the other reconstructions of this study, uses the cell mean and fourth-order approximation to the left and right cell boundary values. The ABC03 parabolic formulation uses the cell mean and second-order estimates of the left and right derivatives in a manner very similar to the PHM of [Marquina \(1994\)](#). Consider an arbitrary cell, I_i , defined on the interval $[x_{i-1/2}, x_{i+1/2}]$ with geometric centre x_i and a grid spacing of $\Delta x_i = x_{i+1/2} - x_{i-1/2}$ with a cell mean of \bar{u}_i , that is:

$$\bar{u}_i \Delta x_i = \int_{x_{i-1/2}}^{x_{i+1/2}} u(x) dx$$

The following three relations constrain a unique parabola, $r_i(x)$, defined on cell I_i :

$$\int_{x_{i-1/2}}^{x_{i+1/2}} r_i(x) dx = \bar{u}_i \Delta x_i$$

$$r_i'(x_i) = d_C$$

$$\begin{cases} r_i'(x_{i-1/2}) = d_L & \text{if } |d_L| \leq |d_R| \\ \text{OR} \\ r_i'(x_{i+1/2}) = d_R & \text{otherwise} \end{cases}$$

The parameters d_L , d_R , and d_C represent second-order approximations to the left, right, and centred derivatives, respectively.

ABC03 chose a polynomial of the global form: $r_i(x) = a_{0,i} + a_{1,i}x + a_{2,i}x^2$, but here a local formulation is used instead: $r_i(x) = a_{0,i} + a_{1,i}(x - x_i) + a_{2,i}(x - x_i)^2$. The coefficients are thus defined as:

$$\begin{cases} a_{2,i} \Delta x_i = d_C - d_L & \text{if } |d_L| \leq |d_R| \\ \text{OR} \\ a_{2,i} \Delta x_i = d_R - d_C & \text{otherwise} \end{cases}$$

$$a_{1,i} = d_C$$

$$a_{0,i} = \bar{u}_i - a_{2,i} \frac{\Delta x_i^2}{12}$$

Note that the lateral derivatives, d_L and d_R must be second-order to achieve third-order reconstruction for sufficiently smooth fields. For unequal grid spacing, the most straightforward approach to second-order derivative estimates is to reconstruct a third-order accurate parabola, $P_3(x)$ across the 3-cell stencil, $I_{i-1} \cup I_i \cup I_{i+1}$, (whose primitive matches the cell means) and differentiate it at the left and right cell boundary locations: $d_L = P_3'(x_{i-1/2})$ and $d_R = P_3'(x_{i+1/2})$. This polynomial $P_3(x)$ is identical to $P_{EXACT}(x)$ in Appendix A. Additionally, for any method which uses second-order lateral derivative approximations for reconstruction (e.g. PHM and PDHM), this is how those derivatives are computed in the meridional direction.

Now, the centred derivative estimate, d_C , is all that is left to calculate. This estimate is what acts to limit the local total variation (LTV) of the parabola to achieve an essentially non-oscillatory reconstruction. A naive choice

would be the simple arithmetic mean, $d_C = (d_L + d_R) / 2$, but this does not bound the LTV. ABC03 used instead the harmonic mean of [Marquina \(1994\)](#):

$$d_C = \min(d_L, d_R) (|d_L| + |d_R|) \frac{|d_L| |d_R|}{|d_L| + |d_R| + \varepsilon}$$

where ε is a machine precision number used to avoid a floating point divide-by-zero and

$$\begin{cases} \min(d_L, d_R) = \text{sign}(d_L) & \text{if } |d_L| \leq |d_R| \\ \text{OR} \\ \min(d_L, d_R) = \text{sign}(d_R) & \text{otherwise} \end{cases}$$

This provided a satisfactorily limited parabola. More recently, however, a generalised mean, Powereno $_p$, (see [Serna and Marquina, 2004](#) and [Serna, 2006](#)) has been developed defining the centred derivative as a power-limited mean of the lateral derivatives given by:

$$d_C = \min(d_L, d_R) \frac{|d_L| + |d_R|}{2} \left(1 - \frac{|d_L| - |d_R|}{|d_L| + |d_R| + \varepsilon} \right)^p \quad (1)$$

where p is a parameter controlling the local variation of the reconstruction. It was shown in [Serna and Marquina \(2004\)](#) that increasing p acts to increase the LTV of hyperbolas asymptotically to that of using an arithmetic mean as $p \rightarrow \infty$, and the same is true for parabolas. Therefore, we adopt the power limiter instead of the ABC03 harmonic limiter in this study with $p = 4$ to allow more local variation while still keeping the parabolas limited.

2.3 Modified Piecewise Parabolic Method (M-PPM)

It is well known that the original PPM limiter of [Colella and Woodward \(1984\)](#) degrades the reconstruction to first-order accuracy at all extrema in order to preserve monotonicity. Recently, a modified limiter for PPM was developed in [Colella and Sekora \(2008\)](#) for uniform grid spacing. This limiter gives improved accuracy at extrema via a non-oscillatory (not strictly monotonic) limiting based on second derivative information. However, the extension of this limiter to a non-uniform grid spacing is not trivial.

Therefore, here we present a new and different approach to improved PPM accuracy at extrema wherein smooth extrema are reconstructed at full accuracy and non-smooth extrema are limited to avoid spurious oscillations. To mathematically indicate the presence of a jump discontinuity at either the left or the right cell boundary, we define a ‘‘jump severity indicator’’, S , identical to exponentiated term in (1):

$$S = \left| \frac{|d_L| - |d_R|}{|d_L| + |d_R| + \varepsilon} \right| \quad (2)$$

Taking a geometric approach, if the *magnitude* of the first derivative changes very abruptly across a cell, that is a solid indicator of a jump discontinuity at which reconstructions tend most to oscillate. This indicator in essence

gives an estimate of the second derivative magnitude confined to the normalised domain: $S \in [0, 1]$. $S = 1$ indicates a strong jump discontinuity, and $S = 0$ indicates a very smooth function.

We want to reconstruct at full accuracy for smooth extrema and at first-order accuracy for non-smooth extrema. Consider the classically limited left and right interface values, u_{lim}^- and u_{lim}^+ , respectively. Also consider the left and right original interpolated interface values, u_{orig}^- and u_{orig}^+ , respectively. We thus, define the left and right interface values used in the final interpolation, u_*^- and u_*^+ , respectively as follows:

$$u_*^\pm = C_S u_{lim}^\pm + (1 - C_S) u_{orig}^\pm \quad (3)$$

where C_S is any functional mapping of S to the same domain: $C_S \in [0, 1]$ with $C_S = 0$ indicating a strong jump discontinuity and $C_S = 1$ indicating smooth data (the reverse of S itself). The purpose of C_S is to control the reconstruction's variation by specifying the sensitivity of the limiting to the value of the severity indicator, S . For example, the [Serna \(2006\)](#) hyperbolas use the mapping $C_S(S) = 1 - S^3$ (i.e. the Powereno₃ limiter), proving that it allows more variation than the [Marquina \(1994\)](#) hyperbolas which use the formal equivalent of the mapping $C_S(S) = 1 - S^2$. We found that a much higher values of p can be used for this reconstruction for most cases. However, in the most severe of jumps ($S \approx 1$), we found the need for a more conservative mapping. Therefore, we used the following mapping for our study to get accuracy when possible and limit oscillations in the severe cases:

$$C_S(S) = \begin{cases} 1 - S^6 & \text{if } S \leq 0.9 \\ 1 - S^3 & \text{if } S > 0.9 \end{cases}$$

There are two cases in which the parabolas of [Colella and Woodward \(1984\)](#) are limited. The first case (which has already been discussed above) is in the presence of extrema (i.e. $(u_{orig}^+ - \bar{u})(\bar{u} - u_{orig}^-) < 0$). The second case is when the data itself is monotonic but the reconstructed parabola is not monotonic within the cell domain. [Colella and Sekora \(2008\)](#) note that the requirement of fully monotonic parabolas within each cell domain in [Colella and Woodward \(1984\)](#) is sufficient but not necessary in order to obtain a monotonic reconstruction. In other words, the original limiting is more restrictive than formally necessary for monotonicity. The convex combination in (3) need not be restricted to extrema alone but can be used (and is used in this study) for *all* cases in which the original parabola is being limited to provide less restrictive non-oscillatory parabolas.

The last modification of the classical PPM is to change the original calculation of interface values. [Colella and Woodward \(1984\)](#) calculated fourth-order accurate monotonic estimates of the interface values over the grid first and then used those for cell reconstruction in a second loop. [Colella and Sekora \(2008\)](#) revised the interface values to be sixth-order accurate, of course, using a

six-cell stencil for each interface. These schemes calculate continuous interface values in one loop and then reconstruct the cells in another loop using those values. Our scheme, on the other hand, calculates both the interface values and the reconstruction in the same loop, rendering two discontinuous values for each interface even without limiting. A comparison in terms of CPU times will later show that this is only a slight overhead in terms of compute time.

We utilise the full five-cell stencil to reconstruct a polynomial and then sample it at the cell interfaces. We cannot always use a fifth-order accurate reconstruction, however, because if there exists a discontinuity in the left-most or right-most cell, the polynomial will oscillate. Given that the limiting based on (2) only takes into account a three-cell stencil, this could lead to uncontrolled oscillations. Therefore, we calculate jump severity indicators from (2) for the cells to the left and right of the centre cell (S_L and S_R , respectively). If S_L or S_R exceed a threshold, S^* , there may be a discontinuity outside the centred three-cell stencil. Therefore, we adapt the stencil of the polynomial to remove any discontinuity which may lie in the left-most or right-most cell. This is described in more detail in Appendix B. A threshold value of $S^* = 0.8$ was experimentally determined and used. The interface values are not limited to be monotonic. Rather, they are subjected to the same constraint given in (3) where, in this case, u_{orig}^\pm and u_{lim}^\pm represent the the sampled polynomial values and the monotonically limited values respectively.

The only modifications to the original PPM of [Colella and Woodward \(1984\)](#) are in the calculation and limiting of interface values. The following steps summarise the process which is performed for each cell to complete the reconstruction.

1. Calculate the severity indicator defined by (2)
2. Construct a polynomial across a five-cell stencil using the method described in Appendix B.
3. Sample the polynomial at the left and right cell boundaries to obtain fifth-order accurate interface values.
4. Calculate monotonically limited estimates of these interface values which are restricted to the range of the neighbouring cell means.
5. Calculate a convex combination of the interface values from step 3, u_{orig}^\pm , and the monotonic values from step 4, u_{lim}^\pm , using (3).
6. Following [Colella and Woodward \(1984\)](#), determine if this cell contains a local extremum or if the parabola constructed from the left and right interface values and cell mean is non-monotonic. If so, calculate the limited value.
7. Calculate a convex combination of the interface values from step 5, u_{orig}^\pm , and the monotonically limited values from step 6, u_{lim}^\pm , again using (3).
8. Using the interface values from step 7 and the cell mean, construct a parabola following [Colella and Woodward \(1984\)](#).

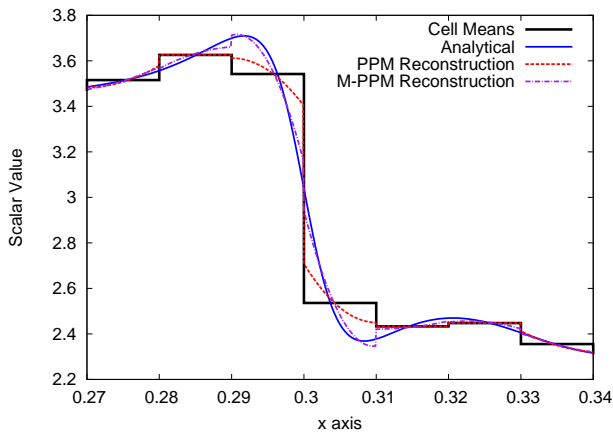


Figure 1. A prescribed irregular signal profile comparing the PPM and the M-PPM reconstructions.

This modification of PPM (which we will denote M-PPM) is not strictly monotonic like PPM but is non-oscillatory like the other methods in this paper. The M-PPM approach here is similar to that of [Blossey and Durran \(2008\)](#) in the sense that the original PPM limiter is only used for parabolas deemed oscillatory by a given formulaic indicator of non-smoothness. There is one main difference, however. The present work uses a functional mapping of the severity indicator to give a convex combination of the limited and unlimited solutions, and [Blossey and Durran \(2008\)](#) used a thresholding technique to determine if parabolas which should be limited. This difference is similar in nature to the difference between ENO and WENO schemes (see [Harten et al., 1987](#) and [Liu et al., 1994](#)).

To show a visual perspective of the effects of the M-PPM modifications in practise, Fig. 1 shows a zoomed plot of a 1-D irregular signal profile (same as in [Norman and Nair, 2008](#)) along with the PPM reconstruction, M-PPM reconstruction, and the analytical profile. In the plot, we have an unresolved gradient and a local maximum in the data to show the relative advantages.

2.4 Weighted Essentially Non-Oscillatory Methods (WENO23 and WENO35)

This form of non-oscillatory approximation originates from papers such as [Harten et al. \(1987\)](#), [Shu and Osher \(1988\)](#), and [Liu et al. \(1994\)](#). The basic idea is as follows. First, create multiple polynomial approximations within different stencils, all of which must include the domain of the target reconstruction cell. Next, estimate the smoothness of each of the polynomials with a formula similar to total variation but for both first- and second-derivatives. Finally, compute weights based on the smoothness indicators such that the smoother polynomials are weighted more than the non-smooth polynomials. A detailed discussion of the WENO reconstruction philosophy is given in [Shu \(1999\)](#).

First, we will discuss WENO23 which is second-order accurate in the worst case and third-order accurate in the best case. The particular implementation used in

this study is very similar to that of [Kurganov and Levy \(2000\)](#). The only difference is that here, the grid spacing is not uniform in the meridional direction on the (λ, μ) -grid (see [Nair and Machenhauer 2002](#)). Therefore, the polynomials themselves and the smoothness indicators must be rederived with this in mind, given in Appendix A. The parameter, p , in [Kurganov and Levy \(2000\)](#) on is set to $p = 1/2$ and is found to bound the total variation satisfactorily. A lower value of p essentially allows more variation in the WENO23 reconstruction and converges more quickly to the optimal accuracy as data smoothness increases.

The WENO35 method which is third-order accurate in the worst case and fifth-order accurate in the best case is derived using similar principles as the WENO23 method. Four polynomials are defined: one fourth-order polynomial defined across a five-cell stencil centred about the target reconstruction cell, one second-order polynomial defined on the left-most three cells, and one second-order polynomial defined on the right-most three cells. Then, the smoothness of each polynomial is evaluated with a total variation estimate applied to all existing derivatives in the approximations. Next, the weights are formed based on the smoothness indicators with the smoothest functions weighted the most. Finally, the weights yield a convex combination of the three polynomials to yield a final reconstruction that is non-oscillatory near shocks yet fifth-order accurate in the presence of smooth data. This implementation is fully described in detail in the reconstruction section of [Capdeville \(2008\)](#). The only way the present implementation differs is in the calculation of the weights. After calculating the smoothness indicators, IS_j , [Capdeville \(2008\)](#) creates weights defined by: $w_j = (\epsilon + IS_j)^{-2}$. We use a similar approach to [Kurganov and Levy \(2000\)](#) and define them as $w_j = (\epsilon + IS_j)^{-p}$ using $p = 1/2$.

It is worth noting that the accuracy of WENO23 and WENO35 is strongly dependent upon the value of p which controls how quickly the reconstruction converges to full-order accuracy as the smoothness indicators converge to equal values. The value of $p = 1/2$ is used here instead of the standard $p = 2$ because it seems to render much better accuracy while still controlling the violation of monotonicity to a sufficiently small magnitude (1-2% in the worst cases).

We found through experimentation that if a particularly strong jump discontinuity exists in the centre cell, all four polynomial interpolants will oscillate strongly. This can cause relative overshoot magnitudes of 10-20% in the CCS context which is highly unacceptable in a non-oscillatory scheme. This is much less severe in the WENO23 scheme as the polynomial orders are lower. To mitigate this effect we experimentally determined the jump severity indicators at which WENO35 oscillates unacceptably and use WENO23 instead in a hybrid fashion. We found that if we use WENO23 instead of WENO35 for $S > 0.98$, the oscillations are much better controlled without greatly affecting the accuracy of the overall WENO35

method. The calculation of S is very cheap, so there is no measurable computational overhead associated with this modification.

3 Test Cases

Four types of global spherical data are used for test cases in this study, all of them adopted from [Lauritzen and Nair \(2008\)](#). The first two test data are originally from [Jones \(1999\)](#) giving one smooth and one spurious harmonic function. The smooth function denoted Y_2^2 and the high frequency function denoted Y_{32}^{16} are defined as:

$$Y_2^2 = 2 + \cos^2 \theta' \cos(2\lambda')$$

$$Y_{32}^{16} = 2 + \sin^{16}(2\theta') \cos(16\lambda')$$

where (λ', θ') are the coordinates on a sphere that is rotated relative to the true sphere. This rotation is a feature provided to avoid symmetry on the grid and place the data in locations (typically the poles) that reveal errors on the grid. Both the Y_2^2 data and the Y_{32}^{16} data have the rotated sphere's pole located at 0° longitude and 45° latitude on the true sphere. These are shown in Fig. 2a and Fig. 2b. Note that the 45° latitude rotation places the Y_{32}^{16} spurious belt passing through the poles. The third test case data produces a vortex at both poles of a rotated sphere. It is defined exactly as in [Lauritzen and Nair \(2008\)](#) with the poles of the rotated sphere located at 0° longitude and 81° latitude. The vortex data is shown in Fig. 2c.

The fourth test case implements a slotted cylinder on the sphere located at the equator. The slotted cylinder originates from [Zalesak \(1979\)](#) and was implemented on the sphere in [Nair et al. \(2003\)](#). It is intended to test a scheme's behaviour in the presence of a multidimensional data jump discontinuity. First, a radius is specified in terms of the rotated latitude and longitude: $R = \sqrt{(\lambda')^2 + (\theta')^2}$. Then, the analytical profile is as follows:

$$Y = \begin{cases} 0 & \text{if } R > \frac{10\pi}{64} \\ 0 & \text{if } R \leq \frac{10\pi}{64} \text{ and } |\lambda'| < \frac{10\pi}{192} \text{ and } \theta' > -\frac{10\pi}{192} \\ 1 & \text{if } \text{otherwise} \end{cases}$$

Quadrature is not used for this test case because we want the profile to be as sharp as possible. Thus, cell centroid values are used to make sure there is a discontinuous jump from zero to unity. For this reason, the only error norms which are valid are the L_{min} and L_{max} norms (which manifest oscillations) because we know the data range is always between zero and unity.

Each of the seven subgrid approximations are tested for intercomparison with the following standard global error norms: L_1 , L_2 , L_∞ , L_{min} , and L_{max} . The formulae are given in [Lauritzen and Nair \(2008\)](#). To briefly discuss the properties of the different error measures, L_1 expresses the most straightforward error measure giving the mean absolute error normalised by the average magnitude of the exact data. L_∞ expresses the largest magnitude of error on the grid normalised by the largest magnitude of the exact

data. Most notably for L_{min} , a negative value indicates violation of positivity. Both L_{min} and L_{max} are normalised by the range of the exact data. L_2 , closely related to root mean squared error, is the 2-norm of the absolute error normalised by the 2-norm of the exact data rendering a larger weighting for larger errors.

For all four data profiles and all eight approximations, two conservative interpolations will be performed for intercomparison. First, the data will be interpolated from a 2° grid to a T42 grid ($\approx 2.8^\circ$ grid spacing) to test the accuracy and oscillatory properties in a coarsening interpolation. Then, the reverse will be performed to test the same properties in a sharpening interpolation. To avoid the need to analytically integrate these complex functions in even more complex rotated coordinates, a five-point Gaussian quadrature is used to obtain cell mean estimates of order much higher than the order of interpolation, thus retaining a meaningful error measure for intercomparison.

4 Numerical Results

PPM will serve as a baseline for comparison due to its general acceptance and use in the atmospheric modelling community. No positive definite filter is used in this study for the purpose of observing the natural potential of each function to violate positivity. For the reader's convenience, a comparative bar chart of L_1 error is given in Fig. 3 to get a quick overall perspective of accuracy.

Considering the very smooth harmonic data, Y_2^2 , (Table II) in a coarsening interpolation, the only methods performing worse than PPM are PRM and WENO23 by a slight margin. It appears from the L_{min} and L_{max} norms that PPM is experiencing undershoots and overshoots. However, this is not because PPM isn't monotonic but because the 2° exact cell means have a larger range than the T42 exact cell means due to the higher resolution of the analytical function. In particular, the L_∞ norm for M-PPM shows that it is resolving the smooth extrema much better than the other methods. In the sharpening interpolation for this same data, as expected, the error norms are larger. The most notable result is that PDHM easily stands out as the most accurate interpolant by an order of magnitude. The advantages of M-PPM are much less pronounced in the sharpening interpolation.

Moving on to the less smooth harmonic data, Y_{32}^{16} , (Table III) in the coarsening interpolation we see violations of positivity on the order of 0.1% much of which, again, is due to the higher resolution of extrema in the exact 2° data profile. Here, M-PPM and WENO35 separate themselves as the most accurate reconstructions for a non-smooth function with a large number of spurious extrema. Most notable is the improvement in the L_∞ norm for M-PPM, evidencing better resolution of the sharp extrema. For the sharpening interpolation, we have violations of positivity on the order of 1% (1.6% max), and only PHM and P-PPM violated monotonicity in this case. Once again, WENO35 and M-PPM separate themselves as the most accurate reconstructions.

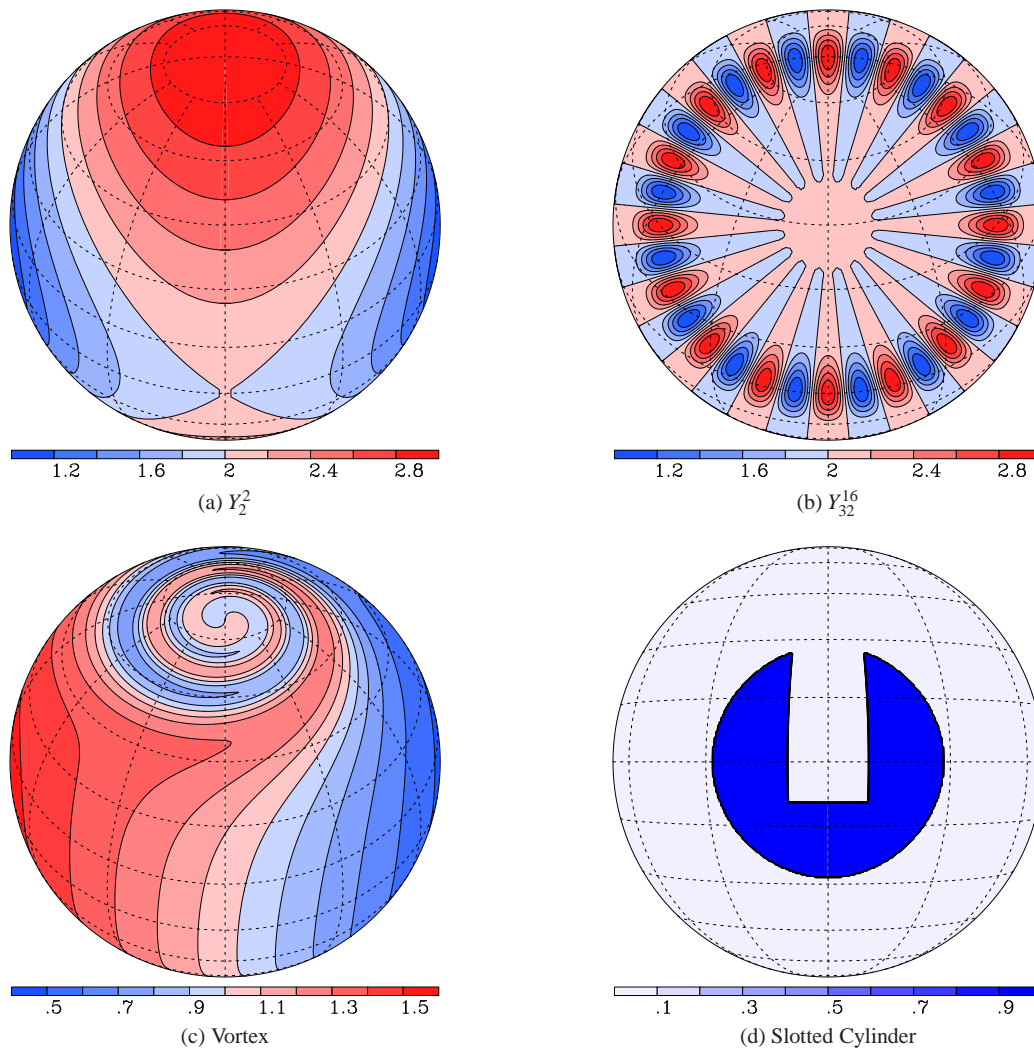


Figure 2. Analytical plots of the three data profiles used in this study.

	2° interpolated to T42					T42 interpolated to 2°				
	L_1	L_2	L_∞	L_{min}	L_{max}	L_1	L_2	L_∞	L_{min}	L_{max}
PPM	2.46E-06	6.14E-06	6.25E-05	-3.09E-05	4.69E-05	3.87E-05	1.01E-04	4.75E-04	5.95E-04	-2.98E-04
PHM	1.25E-06	2.14E-06	8.47E-06	9.61E-06	-2.39E-07	3.35E-05	8.70E-05	3.97E-04	5.95E-04	-2.98E-04
PDHM	3.08E-07	3.93E-07	7.55E-07	4.78E-07	0.00E+00	1.98E-06	1.25E-05	3.92E-04	3.22E-06	-2.75E-04
PRM	2.51E-06	5.97E-06	5.81E-05	-2.96E-05	4.37E-05	3.89E-05	9.99E-05	4.72E-04	5.95E-04	-2.98E-04
P-PPM	6.25E-07	9.73E-07	3.70E-06	5.55E-06	0.00E+00	3.29E-05	8.80E-05	3.97E-04	5.95E-04	-2.98E-04
WENO23	2.60E-06	4.71E-06	2.08E-05	3.12E-05	0.00E+00	3.02E-05	7.34E-05	3.79E-04	5.43E-04	-2.74E-04
WENO35	2.27E-07	3.54E-06	7.88E-05	0.00E+00	5.92E-05	2.86E-05	8.27E-05	3.79E-04	5.43E-04	-2.74E-04
M-PPM	4.75E-08	6.74E-08	1.19E-07	0.00E+00	0.00E+00	3.20E-05	8.96E-05	3.97E-04	5.95E-04	2.46E-06

Table II. Error norms for Y_2^2 test case.

The vortex data test case (Table IV) for the coarsening interpolation shows little in the way of monotonicity violation. WENO35 and M-PPM have the lowest error norms. As typically seems to be the case, PRM is similar to PPM but slightly less accurate. This is likely because they use the same interface values. In the sharpening case, there are no violations of monotonicity manifested by the error norms. Like the coarsening interpolation, WENO35 and M-PPM perform the best with M-PPM slightly less

accurate overall.

As mentioned in section 3, the slotted cylinder test case is intended to challenge the ability of a reconstruction to control oscillations with strong jump discontinuities. The magnitudes of these oscillations are manifested in the L_{min} and L_{max} norms. For both the coarsening and sharpening interpolations, the oscillation magnitudes for all of the methods were order 1% or less. The worst violation occurred with M-PPM which had an undershoot

	2° interpolated to T42					T42 interpolated to 2°				
	L_1	L_2	L_∞	L_{min}	L_{max}	L_1	L_2	L_∞	L_{min}	L_{max}
PPM	7.80E-04	2.06E-03	1.27E-02	1.19E-02	1.56E-03	3.78E-03	9.37E-03	4.99E-02	2.59E-02	-9.47E-03
PHM	1.39E-03	3.45E-03	1.50E-02	1.38E-02	1.89E-05	5.74E-03	1.37E-02	5.49E-02	6.39E-03	1.56E-02
PDHM	7.86E-04	2.02E-03	1.38E-02	1.37E-02	1.44E-05	3.28E-03	8.24E-03	5.42E-02	2.24E-02	-9.42E-03
PRM	8.26E-04	2.15E-03	1.30E-02	1.08E-02	1.40E-03	4.03E-03	9.84E-03	5.04E-02	9.84E-03	-6.37E-03
P-PPM	1.38E-03	3.45E-03	1.50E-02	1.33E-02	1.41E-05	5.69E-03	1.37E-02	5.50E-02	5.72E-03	1.64E-02
WENO23	9.15E-04	2.27E-03	1.28E-02	1.42E-02	-1.09E-05	3.58E-03	8.73E-03	4.89E-02	2.78E-02	-9.40E-03
WENO35	1.17E-04	4.84E-04	1.01E-02	7.00E-05	1.99E-03	1.04E-03	3.92E-03	4.59E-02	1.55E-03	-8.21E-03
M-PPM	1.89E-04	6.65E-04	7.31E-03	1.74E-03	3.37E-06	1.37E-03	4.52E-03	4.56E-02	3.45E-03	-9.45E-03

Table III. Error norms for Y_{32}^{16} test case.

	2° interpolated to T42					T42 interpolated to 2°				
	L_1	L_2	L_∞	L_{min}	L_{max}	L_1	L_2	L_∞	L_{min}	L_{max}
PPM	2.17E-04	9.48E-04	1.00E-02	-3.28E-06	3.33E-06	9.73E-04	3.75E-03	3.24E-02	1.85E-04	-1.85E-04
PHM	3.96E-04	1.58E-03	1.18E-02	-1.92E-05	1.92E-05	1.58E-03	5.69E-03	4.01E-02	2.59E-04	-2.59E-04
PDHM	2.65E-04	1.01E-03	1.05E-02	-2.78E-08	1.11E-07	9.43E-04	3.47E-03	3.40E-02	0.00E+00	0.00E+00
PRM	2.38E-04	1.02E-03	1.02E-02	-9.36E-06	9.44E-06	1.08E-03	4.15E-03	3.16E-02	2.06E-04	-1.68E-04
P-PPM	3.95E-04	1.57E-03	1.17E-02	-1.88E-05	1.88E-05	1.57E-03	5.67E-03	4.00E-02	2.56E-04	-2.56E-04
WENO23	2.96E-04	1.11E-03	1.02E-02	8.55E-06	-8.55E-06	1.04E-03	3.86E-03	3.21E-02	1.01E-04	-1.01E-04
WENO35	6.81E-05	3.08E-04	4.46E-03	0.00E+00	0.00E+00	4.17E-04	1.85E-03	2.93E-02	0.00E+00	0.00E+00
M-PPM	9.12E-05	4.17E-04	7.36E-03	0.00E+00	0.00E+00	5.25E-04	2.19E-03	2.70E-02	1.02E-04	-1.02E-04

Table IV. Error norms for Vortex test case.

of 1.8% in the sharpening interpolation. To give a frame of reference for this test case, when using only the optimal polynomial of WENO35, an overshoot of 32% occurred.

Accuracy alone does not determine efficiency but also runtime and scalability, the most straightforward of which is runtime. To consider this, Table V lists the runtimes of each of the methods for the vortex test case interpolating from a $1/3^\circ$ grid (1080x540) to a $1/2.5^\circ$ grid (900x450). The codes have been optimised, avoiding exponentiation whenever possible and replacing repeated operations with precomputed variables. Clearly, PRM and P-PPM separate themselves as the cheapest reconstructions in terms of speed. WENO35 is clearly more expensive than any of the other methods, yet it also tends to give the best accuracy. It is possible that the runtime may be improved via vectorisation for both WENO35 and WENO23 as they make use of several matrix-vector products during the reconstruction. M-PPM actually requires about 7% more computation than PPM while typically giving much greater accuracy using the same stencil.

Now, regarding scalability the three-cell methods have the potential to scale more efficiently to a larger number of processors than do the five-cell methods due to a reduced communication burden per remapping. As shown in Table I, PHM, PDHM, P-PPM, and WENO23 are the three-cell stencil methods (requiring a 1-cell halo when parallelised), and PPM, M-PPM, PRM, and WENO35 are the five-cell stencil methods (requiring a 2-cell halo when parallelised).

5 Conclusions

An intercomparison of various sub-gridscale functional approximations has been performed in the context of conservative cascade interpolation on a latitude-longitude grid. Eight sets of test cases have been performed interpolating four data profiles both from a T42 grid to a 2° grid and from a 2° grid to a T42 grid to measure the accuracy and oscillation properties of the functions. For all test cases, PDHM generally gives the best accuracy of the three-cell stencil methods. It seems unlikely that the economy of P-PPM would outweigh its comparative lack of accuracy compared to PDHM. WENO35 gives the best accuracy of the five-cell stencil methods, but requires the most computation. M-PPM seems to be a good alternative to WENO35 with a large decrease in computational burden and a small relative decrease in accuracy.

Caution should be taken when using a non-oscillatory method that is not strictly monotonic to ensure that the orders of magnitude of monotonicity and positivity violation reported herein (order 1%) are within acceptable bounds. A post-processing positive definite filter may be employed to ensure no negative values are produced in the interpolation for positive species. Note also that tunable parameters of the non-oscillatory reconstructions M-PPM, WENO23, WENO35, PDHM, PHM, and P-PPM may be tweaked for a particularly sensitive application until the oscillations are satisfactorily controlled for representative data. All sub-grid reconstructions in this study could be implemented in any conservative remapping algorithm employing 1-D sweeps such as the conservative cascading implemented in cubed sphere geometry

Method	PPM	PHM	PDHM	PRM	P-PPM	M-PPM	WENO23	WENO35
Runtime (sec)	2.528	2.446	2.691	2.169	1.961	2.713	2.401	3.504
% deviation from PPM	—	-3.2%	+6.4%	-14.2%	-22.4%	+7.3%	-5.0%	+38.6%

Table V. Runtimes in seconds and percent deviation from PPM runtime for the vortex test case interpolating from a $1/3^\circ$ grid to a $1/2.5^\circ$ grid.

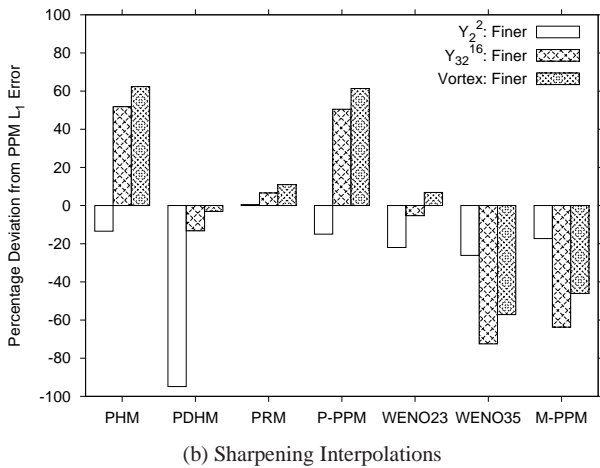
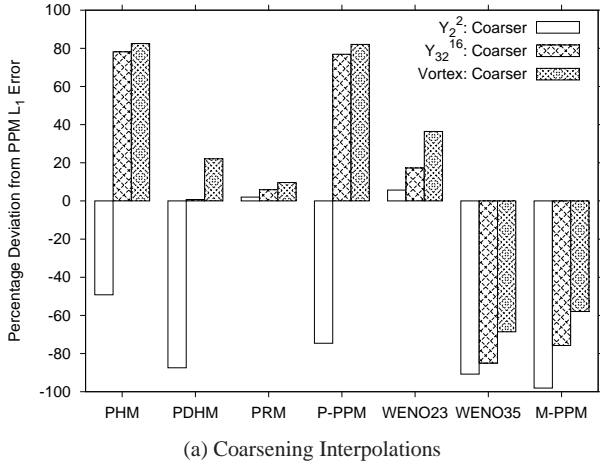


Figure 3. Percentage Deviation of L_1 error from PPM for the Y_2^2 , Y_{32}^{16} , and vortex test cases. ‘‘Coarser’’ denotes an interpolation from a 2° grid to a T42 grid, and ‘‘Finer’’ denotes the reverse.

(Lauritzen and Nair, 2008).

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Appendix A

Here, the WENO23 method will be updated from the one defined in Kurganov and Levy (2000) for a non-uniform grid spacing. We define cell I_i to have grid spacing Δx_i defined within $[x_{i-1/2}, x_{i+1/2}]$ with geometric centre x_i , cell mean \bar{u}_i . Following the notation of Kurganov and Levy (2000), we here define the three polynomials $P_{i,L}(x)$, $P_{i,R}(x)$, and $P_{i,EXACT}(x)$ for an arbitrary cell of index i . Recall that $P_{i,C}(x)$ is defined purely as a function of $P_{i,L}$, $P_{i,R}$, and $P_{i,EXACT}$. In a point-wise framework, polynomial reconstruction must match point values, but in the finite volume framework, cell means must be replicated requiring use of the polynomial’s primitive. The primitive reconstruction principle of Harten et al. (1987) which is consistent with the finite volume formulation gives the following three relations to constrain the coefficients of

$$P_{i,EXACT}(x) = s_{i,0} + s_{i,1}(x - x_i) + s_{i,2}(x - x_i)^2;$$

$$\int_{x_i - \Delta x_i/2}^{x_i - \Delta x_i/2 - \Delta x_{i-1}} P_{i,EXACT}(x) dx = \bar{u}_{i-1} \Delta x_{i-1}$$

$$\int_{x_i - \Delta x_i/2}^{x_i + \Delta x_i/2} P_{i,EXACT}(x) dx = \bar{u}_i \Delta x_i$$

$$\int_{x_i + \Delta x_i/2}^{x_i + \Delta x_i/2 + \Delta x_{i+1}} P_{i,EXACT}(x) dx = \bar{u}_{i+1} \Delta x_{i+1}$$

Integration yields a system of equations of the form: $\mathbf{A}\mathbf{s} = \mathbf{u}$ where $\mathbf{s} = [s_{i,0}, s_{i,1}, s_{i,2}]^T$ and $\mathbf{u} = [\bar{u}_{i-1}, \bar{u}_i, \bar{u}_{i+1}]^T$. Therefore, the coefficient vector, \mathbf{c} , is given by $\mathbf{s} = \mathbf{A}^{-1}\mathbf{u}$. The matrix \mathbf{A} is given by:

$$\mathbf{A} = \frac{1}{2} \begin{bmatrix} 2 & -\Delta x_i - \Delta x_{i-1} & \frac{1}{2}\Delta x_i^2 + \Delta x_i \Delta x_{i-1} + \frac{2}{3}\Delta x_{i-1}^2 \\ 2 & 0 & \frac{1}{6}\Delta x_i^2 \\ 2 & \Delta x_i + \Delta x_{i+1} & \frac{1}{2}\Delta x_i^2 + \Delta x_i \Delta x_{i+1} + \frac{2}{3}\Delta x_{i+1}^2 \end{bmatrix}$$

In practise, this matrix inverse is precomputed and a matrix-vector multiply renders the coefficients during runtime. The linear polynomials $P_{i,L}(x) = l_{i,0} + l_{i,1}(x - x_i)$ and $P_{i,R}(x) = r_{i,0} + r_{i,1}(x - x_i)$ are defined similarly but are simple enough to solve without a linear system. The coefficients are as follows: $l_{i,0} = r_{i,0} = \bar{u}_i$, $l_{i,1} = 2(\bar{u}_i - \bar{u}_{i-1}) / (\Delta x_i + \Delta x_{i-1})$, and $r_{i,1} = 2(\bar{u}_{i+1} - \bar{u}_i) / (\Delta x_i + \Delta x_{i+1})$.

The smoothness indicators also must be rederived to account for non-uniform grid spacing though the functional form is quite similar to that given in Kurganov and Levy

(2000). They are as follows (using the same notation):

$$IS_{i,L} = l_{i,1}^2 \Delta x_i^2; \quad IS_{i,R} = r_{i,1}^2 \Delta x_i^2$$

$$IS_{i,C} = c_{i,1}^2 \Delta x_i^2 + \frac{13}{3} c_{i,2}^2 \Delta x_i^4$$

where $c_{i,0}$, $c_{i,1}$, and $c_{i,2}$ are coefficients of $P_{i,C}(x)$.

Appendix B

Here, we describe the process of creating the polynomial used to obtain interface values for M-PPM in step 2 of the summary. We have a five-cell stencil, I_{i-2}, \dots, I_{i+2} , centred on cell i . First, we calculate jump severity indicators, S_L and S_R , centred on cells I_{i-1} and I_{i+1} (respectively) using equation (2). These will detect discontinuities on either cell boundary of cells I_{i-1} and I_{i+1} . If $S_L \geq S^*$, this indicates that there is a sufficiently severe discontinuity on either the left boundary (arising from cell I_{i-2}) or the right boundary (arising from cell I_i). If the discontinuity is on the left boundary, equation (3) does not take cell I_{i-2} into account, and thus the oscillation is not controlled. Same arguments apply for S_R .

If both $S_L < S^*$ and $S_R < S^*$, then we compute a centred, fifth-order accurate, five-cell stencil polynomial on cells $I_{i-2} \dots I_{i+2}$ which is identical to $\bar{u}_{opt}(x)$ of Capdeville (2008). If $S_L \geq S^*$, then we neglect cell I_{i-2} to get rid of the potential discontinuity, computing a right-biased, fourth-order accurate, four-cell stencil polynomial, $P_{i,R4}(x)$, from cells $I_{i-1} \dots I_{i+2}$. Likewise, if $S_R \geq S^*$, we neglect cell I_{i+2} , computing a left-biased, fourth-order accurate, four-cell stencil polynomial, $P_{i,L4}(x)$, from cells $I_{i-2} \dots I_{i+1}$. If both $S_L \geq S^*$ and $S_R \geq S^*$, a centred, third-order accurate, three-cell stencil polynomial (identical to $P_{i,EXACT}(x)$ from Appendix A) is computed using cell $I_{i-1} \dots I_{i+1}$. We use the primitive reconstruction principle of Harten *et al.* (1987) to constrain the polynomial coefficients on the fourth-order accurate polynomials as follows.

$$\int_{x_i - \Delta x_i/2 - \Delta x_{i-1}}^{x_i - \Delta x_i/2 - \Delta x_{i-1}} P_{i,L4}(x) dx = \bar{u}_{i-2} \Delta x_{i-2}$$

$$\int_{x_i - \Delta x_i/2 - \Delta x_{i-1}}^{x_i - \Delta x_i/2} P_{i,L4}(x) dx = \bar{u}_{i-1} \Delta x_{i-1}$$

$$\int_{x_i - \Delta x_i/2}^{x_i + \Delta x_i/2} P_{i,L4}(x) dx = \bar{u}_i \Delta x_i$$

$$\int_{x_i + \Delta x_i/2}^{x_i + \Delta x_i/2 + \Delta x_{i+1}} P_{i,L4}(x) dx = \bar{u}_{i+1} \Delta x_{i+1}$$

$$\int_{x_i - \Delta x_i/2 - \Delta x_{i-1}}^{x_i - \Delta x_i/2} P_{i,R4}(x) dx = \bar{u}_{i-1} \Delta x_{i-1}$$

$$\int_{x_i - \Delta x_i/2}^{x_i + \Delta x_i/2} P_{i,R4}(x) dx = \bar{u}_i \Delta x_i$$

$$\int_{x_i + \Delta x_i/2}^{x_i + \Delta x_i/2 + \Delta x_{i+1}} P_{i,R4}(x) dx = \bar{u}_{i+1} \Delta x_{i+1}$$

$$\int_{x_i + \Delta x_i/2 + \Delta x_{i+1}}^{x_i + \Delta x_i/2 + \Delta x_{i+1} + \Delta x_{i+2}} P_{i,R4}(x) dx = \bar{u}_{i+2} \Delta x_{i+2}$$

These constraints form a linear system just as in Appendix A. However, the matrix is too large to explicitly give here. In practise, this matrix is inverted analytically for accuracy purposes using a program capable of symbolic algebraic manipulation, and it is precomputed so that a matrix-vector multiply renders the polynomial. As can be seen, the polynomial which renders the interface values for M-PPM will be from third-order to fifth-order accurate. Because classical PPM is formally fourth-order accurate when integrated and applied to smooth data and a uniform mesh, it makes sense to try to keep the interface values to fourth-order accuracy or more. We note that the case where the interface values are limited to third-order accuracy which is necessary to ensure bounded oscillations does not occur often in any of our test cases.

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